# **Complex Symmetric Matrices**

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Complex Symmetric Matrices - p. 1/30

## Outline

- Why complex symmetry?
- Properties of complex symmetric matrices
- Projection of complex symmetric matrices
- Structure preservation and the QEP connection

Complex symmetric matrices appear in complex analysis:

- Grunsky inequality (Horn and Johnson):
  - *f* regular analytic on unit disk, normalized
  - Define  $B(z) = B(z)^T$ ,  $A(z) = A(z)^H$  s.t. f is 1-1 iff

$$x^{H}A(z)x \ge |x^{T}B(z)x|$$

for all  $x, z \in \mathbb{C}^n$  s.t.  $|z_i| < 1$ .

- Moment problems (Horn and Johnson)
  - Given  $\{a_0, a_1, \ldots\} \in \mathbb{C}$
  - Define complex symm Hankel matrices  $A_{2n} \in \mathbb{C}^{2n \times 2n}$
  - $a_i$  are Fourier coeff for a bounded function iff for all n

$$|x^T A_{2n} x| \le c x^H x$$
 all  $x \in \mathbb{C}^{2n}$ 

... and in data fitting and quadrature applications:

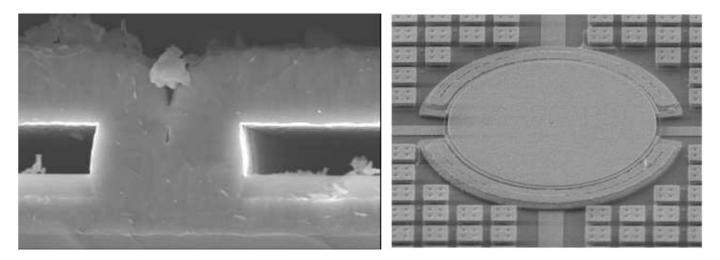
- Exponential fitting (Vandevoore; Luk and Qiao)
  - Given signals  $s_0, \ldots, s_n$
  - Find  $\{a_i\}$ ,  $\{z_i\}$ , and smallest r so

$$s_k = \sum_{i=1}^r a_i z_i^k$$

- Turns into a complex-symm tridiagonal eigenproblem
- Quadrature (Ammar, Calvetti, Reichel)
  - Real symm tridiagonal eigenproblem  $\implies$ Gauss quadrature rules (Golub-Welsch algorithm)
  - Complex-symm tridiagonal eigenproblem ⇒
     Gauss-Kronrod with complex nodes or neg weights Complex Symmetric Matrices - p. 4/30

... and in physical problems with damped resonances:

- Problems with material loss:
  - Viscoelasticity via the Correspondence Principle (e.g. Christensen)
  - EM waveguide simulation in the presence of conductors (e.g. Arbenz and Hochstenbach)
- Infinite domain models:
  - Perfectly matched layer (PML)
    - First in electromagnetics (Berengér 95)
    - Then acoustics, elasticity, etc.
  - Exterior complex scaling in quantum mechanics
    - Invented earlier than PMLs (Simon 79)
    - Same idea, little mutual awareness



My interest: damping in high-freq MEMS resonators

- Want to minimize losses in RF MEMS
- Physics isn't always well-understood
- Want to compute:
  - Damped mode shapes and frequencies
  - Reduced-order models of freq response

### **Damped MEMS resonances**

- Material losses
  - Low intrinsic losses in silicon, diamond, germanium
  - Terrible material losses in metals
- Anchor loss
  - Elastic waves radiate from structure
- Thermoelastic damping
  - Volume changes induce temperature change
  - Diffusion of heat leads to mechanical loss
- Fluid damping
  - Air is a viscous fluid ( $\operatorname{Re}\ll 1$ )
  - Can operate in a vacuum
  - Shown not to dominate in many RF designs

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#### **Viscoelastic losses**

Start with time-harmonic elasticity (weak form):

$$-\omega^2 \int_{\Omega} w \cdot \rho u \, d\Omega + \int_{\Omega} \epsilon(w) : \sigma \, d\Omega = \int_{\Gamma} w \cdot t \, d\Gamma$$

where

- $\checkmark$  u is time-harmonic displacement ( $u^0 = ue^{i\omega t}$ )
- $\epsilon = (\nabla u)^s$  is time-harmonic strain
- $\sigma = C : \epsilon$  is time-harmonic stress
- $\bullet$  t is time-harmonic surface traction

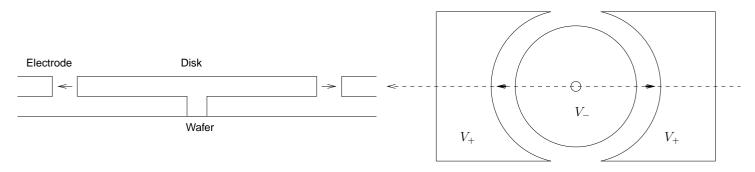
Finite element discretization is real symmetric:

$$-\omega^2 M u + K u = F$$

#### **Viscoelastic losses**

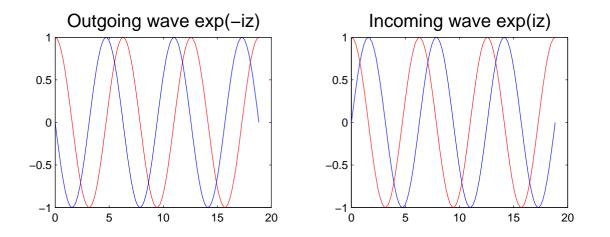
- Viscoelasticity:  $\sigma = \hat{C}(\omega) : \epsilon$ 
  - $\hat{C}(\omega)$  = Fourier transform of relaxation kernel
  - Correspondence principle: hysteresis described through complex-valued material properties
  - Similar principle for acoustics, electromagnetics
- **Simplest case:**  $\hat{C} = C + i\omega\eta I$ 
  - Corresponds to adding a shear viscosity  $\eta$
- Finite element:  $-\omega^2 M u + K(\omega)u = F$ 
  - $K(\omega)$  is complex symmetric
  - Simplest case:  $K(\omega) = K_0 + i\omega D$

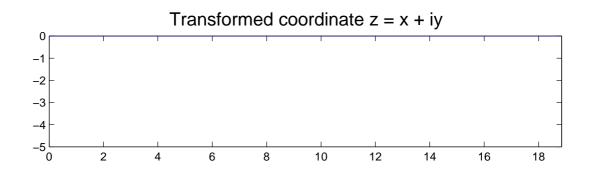
#### **Anchor loss and PMLs**

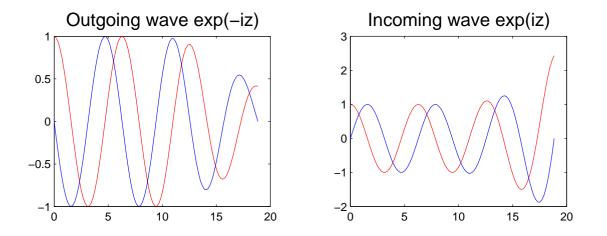


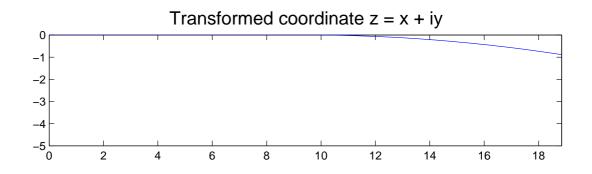
Want to model elastic radiation from resonator to substrate

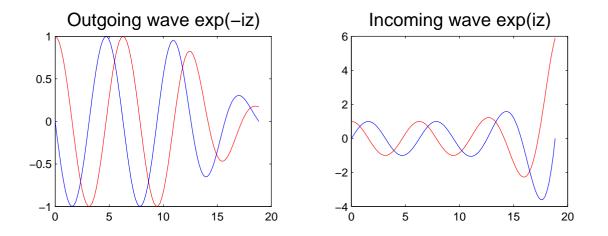
- Apply a complex coordinate transformation
- Generates a non-physical absorbing layer
- No impedance mismatch between the computational domain and the absorbing layer
- Idea works with general linear wave equations

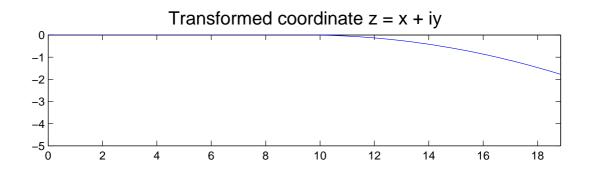


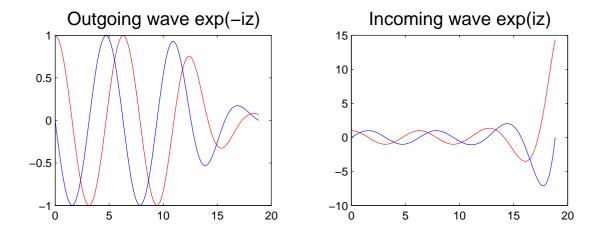


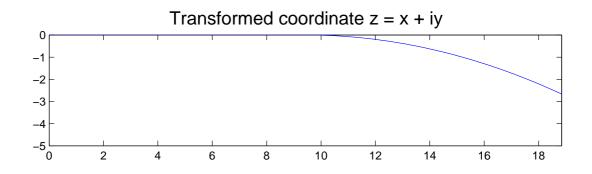


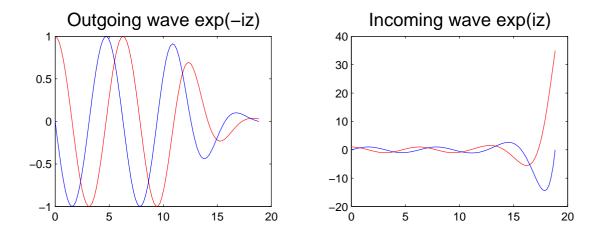


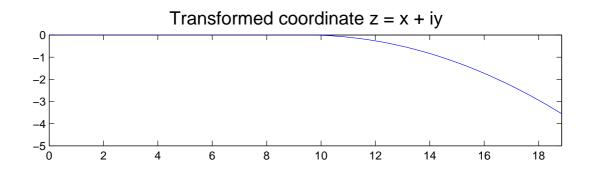


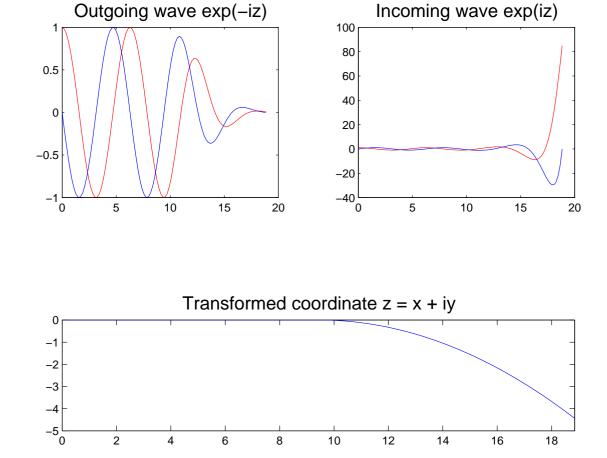












Clamp solution at transformed end to isolate outgoing wave.

#### **Elastic PML**

Weak form of time-harmonic PML equation:

$$-\omega^2 \int_{\Omega} w \cdot \rho u \, \boldsymbol{J} \, d\Omega + \int_{\Omega} \tilde{\boldsymbol{\nabla}} w : \boldsymbol{\mathsf{C}} : \tilde{\boldsymbol{\nabla}} u \, \boldsymbol{J} \, d\Omega = \int_{\Omega} w \cdot t \, d\Gamma$$

- J is the Jacobian of the transformation,  $\tilde{\nabla}$  is the transformed gradient operator
- Coordinate transform typically depends on  $\omega$ 
  - Needed to make decay frequency-independent
- Finite element:  $-\omega^2 M(\omega)u + K(\omega)u = F$ 
  - *M* and *K* now *both* complex symmetric

#### **Eigenvalue problems**

Consider the eigenvalue problem

$$\left(-\omega^2 M(\omega) + K(\omega)\right)u = 0$$

where M and K are complex and may depend on  $\omega$ .

Can get a complex symmetric *linear* eigenproblem by

- Linearizing:  $\omega = \omega_0 + \delta$ , discard  $O(\delta^2)$  terms
- Using  $M(\omega_0)$  and  $K(\omega_0)$ 
  - Makes sense for PML (damping usually adequate for  $\omega$  the same order of magnitude as  $\omega_0$ )
- Good idea when good shift is available

#### **Eigenvalue problems**

Not always approximating nonlinear eigenproblems. Can get eigenvalue problems from separation of variables.

- Continuous translational symmetry
  - Infinite guide, constant cross-section
  - Fixed forcing frequency
- Discrete translational symmetry (Bloch-Floquet waves)
  - SAW filter arrays (Zaglymayr, Sch oberl, Langer)
  - Electromagnetic filters

## **Complex symmetric eigenproblem**

Thm: Every matrix is similar to a complex symmetric matrix.

- Can have arbitrary Jordan structure
- Complex symmetry is still useful

Analogues exist for many statements about Hermitian matrices (see Horn and Johnson, section 4.4).

## **Complex symmetric eigenproblem**

- If z is a column eigenvector, then  $z^T$  is a row eigenvector
- The modified Rayleigh quotient

$$\theta(z) = \frac{z^T K z}{z^T M z}$$

is stationary at eigenvectors (assuming  $z^T M z \neq 0$ ); at an eigenvector,  $\theta$  equals the eigenvalue.

- Eigenvectors for distinct eigenvalues are *complex* orthogonal:  $z^T M w = 0$ .
- But the nice minimax results of the Hermitian case lack analogues here.

## **Ordinary and modified RQ**

$$\ \, \rho(z) = \frac{z^H K z}{z^H M z}$$

- $\{z^H M z = 1\}$  is compact (for M pos def)  $\implies \rho$  has bounded range (field of values)
- Only first-order accurate eigenvalue estimate

$$\theta(z) = \frac{z^T K z}{z^T M z}$$

- $\{z^T M z = 1\}$  is non-compact,  $\theta$  can generally go wild
- Second-order accurate eigenvalue estimate when z is near an eigenvalue

# **Physics of** $z^T z = 0$

The bad case  $z^T M z = 0$  (or  $\approx 0$ ) can happen

- Mimicking infinite domain means we approximate the essential spectrum
- Propogating waves give  $z^T M z \approx 0$  (Olyslager 04)
- Same occurs in quantum mechanical computations
- Usually interested in the discrete part of the spectrum

## **Complex-symmetric projection**

#### Algorithms:

- Complex-symmetric Lanczos (Cullum and Willoughby)
- Arnoldi
- Complex Jacobi-Davidson
- Splitting bases
- Can do spectral transformations (e.g. shift-invert)
- Can start nonlinear eigencomputation from a linear one
- Projections may be used to build reduced models, too

# **Complex-symmetric Lanczos**

• 
$$u_0 = 0, \beta_0 = 0$$
  
• for  $j = 1$  to  $k$   
•  $v := K u_j$   
•  $\alpha_j := u_j^T M v$   
•  $v := v - \alpha_j u_j - \beta_{j-1} u_{j-1}$   
•  $\beta_j := \sqrt{v^T M v}$   
•  $u_{j+1} := v/\beta_j$ 

## **Complex-symmetric Lanczos**

- Half the work, storage of usual non-symmetric Lanczos
- Used for model-reduction (with proportional drive and sense), gets usual PVL matching in 2n moments
- Still has breakdown, near breakdown, woe and doom
- Has been used both for eigenproblems and for solving linear systems (Freund)
- See Eigentemplates section 7.11.

# Arnoldi

- Can compute a unitary (vs complex orthogonal) Krylov subspace basis W using standard Arnoldi
  - Avoids issues with ill-conditioning in the basis
  - But requires work to orthogonalize against more previous vectors
- Once the basis is in hand:
  - Use eigenvalues of  $(W^H K W, W^H M W)$ 
    - Usual nonsymmetric approach
  - Use eigenvalues of  $(W^T K W, W^T M W)$ 
    - Get second-order accuracy when W contains good eigenvector estimates
    - Identical (in exact arithmetic) to estimates from nonsymmetric Lanczos.
  - Could we combine the two?

## **Complex-symmetric Jacobi-Davidson**

- Proposed by Arbenz and Hochstenbach
- Specializes two-sided JD (half the work, storage)
- Uses modified Rayleigh quotient
- Main problem in examples was preconditioning inner solver

# **Basis-splitting**

Let  $W = U + iV \in \mathbb{C}^k$  be a basis (e.g. from Arnoldi)

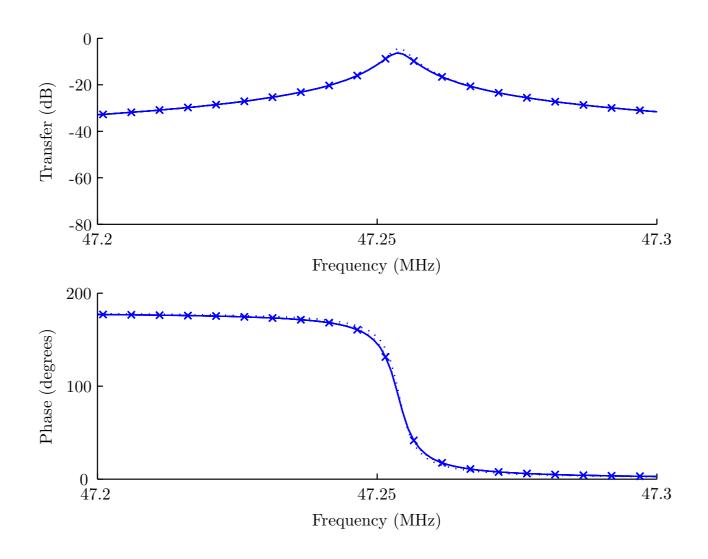
- Form  $Q = \operatorname{orth}([U, V]) \in \mathbb{R}^{n \times 2k}$ 
  - Span of Q contains span of  $[W, \overline{W}]$
- Compute eigenvalues of  $(Q^T K Q, Q^T M Q)$ 
  - Forming  $(Q^T K Q, Q^T M Q)$  not more expensive than projection with W
  - If M is pos def, Ritz values will remain bounded
  - Maintain accuracy of modified Rayleigh quotient

# **Basis splitting**

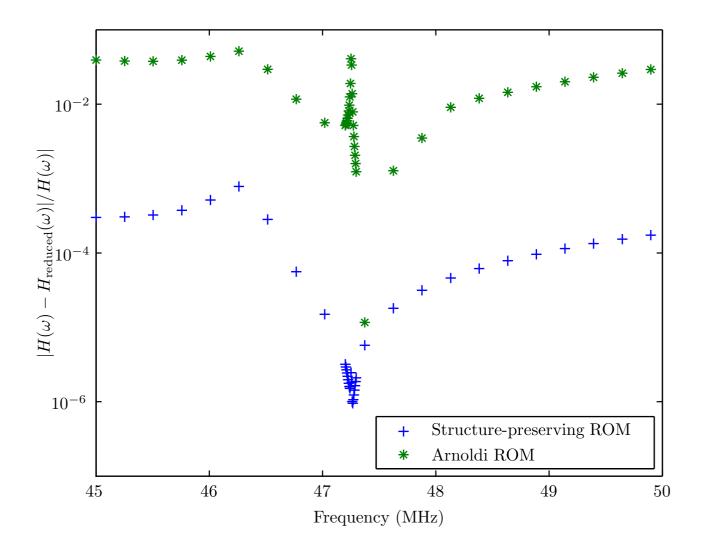
Using the split basis preserves several structures:

- Projected system remains complex symmetric
- Projection doesn't mix up real and imaginary parts
  - Real symmetries of mass, damping, stiffness preserved
- Matches Galerkin discretization of PDEs
  - Like choosing real-valued global shape functions
  - Easier to think about physically
  - Provided the original motivation for this splitting

## **Example: Disk resonator response**



#### **Example: Disk resonator response**



#### **Another relation to the QEP**

Linearize the real QEP  $(\lambda^2 I + \lambda D + K)v = 0$ :

$$\begin{bmatrix} -D & -K \\ I & 0 \end{bmatrix} \begin{bmatrix} v & \bar{v} \\ \lambda v & \bar{\lambda v} \end{bmatrix} = \begin{bmatrix} v & \bar{v} \\ \lambda v & \bar{\lambda v} \end{bmatrix} \begin{bmatrix} \lambda & 0 \\ 0 & \bar{\lambda} \end{bmatrix}$$

Map  $\mathbb{C}$  to  $\mathbb{R}^{2 \times 2}$  in the standard way and consider C = A + iB:

$$\begin{bmatrix} A & -B \\ B & A \end{bmatrix} \begin{bmatrix} z & \bar{z} \\ -iz & -\bar{i}z \end{bmatrix} = \begin{bmatrix} z & \bar{z} \\ -iz & -\bar{i}z \end{bmatrix} \begin{bmatrix} \lambda & 0 \\ 0 & \bar{\lambda} \end{bmatrix}$$

## **Another relation to the QEP**

- For both real form of complex symmetric eigenproblems and QEP, want to preserve structure under projection
  - Probably best to stay within original form
- For both complex symmetric eigenproblems and QEP, may want to split complex projection bases

## Conclusions

- Complex symmetric systems occur in interesting places
  - Particularly in any damped resonant systems
  - Often tangled into nonlinear eigenproblems
- Can pay to exploit complex symmetry when it occurs

Further reading:

- Reduced order models in microsystems and RF MEMS (www.cs/~dbindel/papers/para04.pdf)
- Elastic PMLs for resonator anchor loss simulation (www.cs/~dbindel/papers/pml-tr.pdf)